

Computational Magma Dynamics

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Magma Dynamics Collaboration



Richard Katz

Timestepping Collaboration



Jed Brown

What am I going to talk about?

- Magma Dynamics Model
- FEM formulation and solver
- FEM+FVM formulation and solver

Why is this important?

- It is difficult to compare meshes, discretizations, and multilevel solvers
- **Comparison** is essential for making informed algorithmic choices
- Comparison in a **single code** seems necessary

Outline

- 1 Problem Definition
- 2 Solvers for FEM Formulation
- 3 Solvers for FEM+FVM Formulation

Dimensional Formulation

$$\nabla p - \nabla \zeta_\phi (\nabla \cdot \vec{v}^S) - \nabla \cdot (2\eta_\phi \dot{\epsilon}^S) = 0$$

$$\nabla \cdot \left(-\frac{K_\phi}{\mu} \nabla p + \vec{v}^S \right) = 0$$

$$\frac{\partial \phi}{\partial t} - \nabla \cdot (1 - \phi) \vec{v}^S = 0$$

Closure Conditions

$$K_\phi = K_0 \left(\frac{\phi}{\phi_0} \right)^n$$

$$\eta_\phi = \eta_0 \exp(-\lambda(\phi - \phi_0))$$

$$\zeta_\phi = \zeta_0 \left(\frac{\phi}{\phi_0} \right)^{-m}$$

Nondimensional Formulation

$$\nabla p - \nabla \cdot \left(\left(\frac{\phi}{\phi_0} \right)^{-m} \nabla \cdot \vec{v}^S \right) - \nabla \cdot \left(2e^{-\lambda(\phi - \phi_0)} \dot{\epsilon}^S \right) = 0$$

$$\nabla \cdot \left(-\frac{R^2}{r_\zeta + 4/3} \left(\frac{\phi}{\phi_0} \right)^n \nabla p + \vec{v}^S \right) = 0$$

$$\frac{\partial \phi}{\partial t} - \nabla \cdot (1 - \phi) \vec{v}^S = 0$$

Initial and Boundary conditions

Initially

$$\phi = \phi_0 + A \cos(\vec{k} \cdot \vec{x})$$

where

$$A \ll \phi_0$$

and on the top and bottom boundary

$$K_\phi \nabla p \cdot \hat{n} = 0$$

$$\vec{v}^S = \pm \frac{\dot{\gamma}}{2} \hat{x}$$

Mechanical Benchmarks

Benchmark 0: $\lambda = 0$

There is no porosity feedback, and the initial pattern is stably advected:

$$\vec{k}(t) = \vec{k}_0 \left(\hat{x} \sin \theta_0 + \hat{y} (\cos \theta_0 - t \sin \theta_0) \right)$$

Benchmark 1: $\lambda > 0$

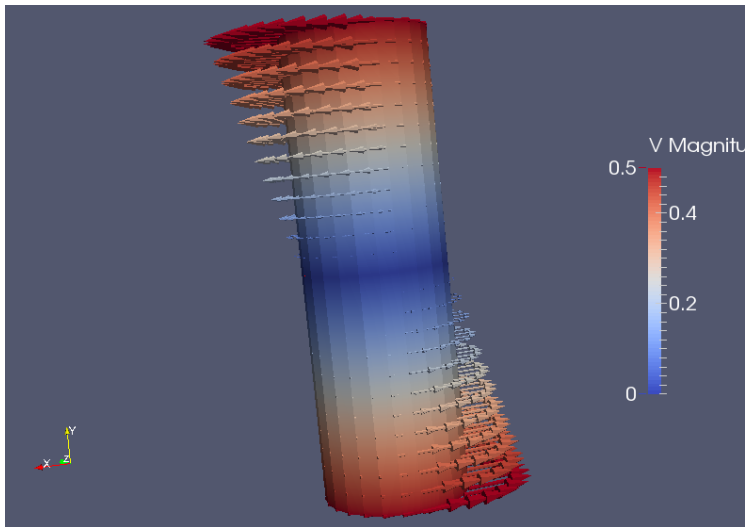
The porosity feedback causes localization, with initial compaction rate:

$$\mathcal{C} = \nabla \cdot \vec{v}_S|_{t=0} = \frac{A\lambda\phi_0 \sin(2\theta_0)}{r_\zeta + 4/3} \cos(\vec{k} \cdot \vec{x})$$

Initial Porosity



Initial Velocity



Outline

- 1 Problem Definition
- 2 Solvers for FEM Formulation**
- 3 Solvers for FEM+FVM Formulation

Mesh

With PETSc's DMplex, we can use

- Simplicies,
- Hexes,
- 2D and 3D,

changing nothing but mesh creation.

I do this in [SNES ex62](#)

PETSc Viewers can output

- Meshes
- Solutions,
- Auxiliary and derived fields,

to HDF5/Xdmf using simple options.

PETSc Viewers can output

```
-dm_view hdf5:sol_fv_1.h5  
-magma_view_solution hdf5:sol_fv_1.h5::append  
-compaction_vec_view hdf5:sol_fv_1.h5:HDF5_VIZ:append
```

to HDF5/Xdmf using simple options.

Discretization

Using continuous FE spaces,

which satisfy an inf-sup stability condition.

Discretization

Using continuous FE spaces,

Q_2 velocity

Q_1 pressure

Q_1 porosity

which satisfy an inf-sup stability condition.

Discretization

Using continuous FE spaces,

```
-velocity_petscspace_order 2
  -velocity_petscspace_poly_tensor
-pressure_petscspace_order 1
  -pressure_petscspace_poly_tensor
-porosity_petscspace_order 1
  -porosity_petscspace_poly_tensor
```

which satisfy an inf-sup stability condition.

Discretization

Using continuous/discontinuous FE spaces,

Q_2 velocity

$P_{1\text{disc}}$ pressure

Q_1 porosity

which satisfy an inf-sup stability condition.

Discretization

Using continuous/discontinuous FE spaces,

```
-velocity_petscspace_order 2
  -velocity_petscspace_poly_tensor
-pressure_petscspace_order 1
  -pressure_petscspace_poly_tensor
  -pressure_petscdualspace_lagrange_continuity 0
-porosity_petscspace_order 1
  -porosity_petscspace_poly_tensor
```

which satisfy an inf-sup stability condition.

Solver Organization

Timestepping

We will use simple Backward Euler:

$$\nabla p^{k+1} - \nabla \left(\left(\frac{\phi^{k+1}}{\phi_0} \right)^{-m} \nabla \cdot \vec{v}^{k+1} \right) - \nabla \cdot \left(2e^{-\lambda(\phi^{k+1} - \phi_0)} \dot{\epsilon}^{k+1} \right) = 0$$

$$\nabla \cdot \left(-\frac{R^2}{r_\zeta + 4/3} \left(\frac{\phi^{k+1}}{\phi_0} \right)^n \nabla p^{k+1} + \vec{v}^{k+1} \right) = 0$$

$$\frac{\phi^{k+1} - \phi^k}{\Delta t} - \nabla \cdot (1 - \phi^{k+1}) \vec{v}^{k+1} = 0$$

Solver Organization

Newton-Krylov

Begin with a Newton-Krylov solve with line search:

$\mathcal{N} \setminus \mathbf{K} - \mathcal{L}$ NRICH

Optimal linear preconditioner in
Rhebergen, Wells, Wathen, and Katz, SISC.

Solver Organization

Newton-Krylov without Porosity

We can separate the Stokes-like solve from the porosity advection:

$$\begin{array}{cc|c}
 A \oplus \text{Schur } L & & 0 \\
 & & 0 \\
 \hline
 F & 0 & I + G
 \end{array}$$

Solver Organization

Newton-Krylov

```
-pc_type fieldsplit
  -pc_fieldsplit_0_fields 0,1 -pc_fieldsplit_1_fields 2
  -pc_fieldsplit_type multiplicative
    -fieldsplit_0_pc_type fieldsplit
    -fieldsplit_0_pc_fieldsplit_type schur
    -fieldsplit_0_pc_fieldsplit_schur_precondition selfp
    -fieldsplit_0_pc_fieldsplit_schur_factorization_type full
    -fieldsplit_0_fieldsplit_velocity_pc_type lu
    -fieldsplit_0_fieldsplit_pressure_ksp_rtol 1.0e-9
    -fieldsplit_0_fieldsplit_pressure_pc_type gamg
    -fieldsplit_0_fieldsplit_pressure_ksp_monitor
    -fieldsplit_0_fieldsplit_pressure_ksp_gmres_restart 100
    -fieldsplit_fieldsplit_0_pressure_ksp_max_it 200
```

Solver Organization

Newton-Krylov with Porosity

Or we can incorporate the porosity advection into the Stokes-like solve:

$$\begin{array}{c|c} \mathbf{A} & \mathbf{E} \\ \hline \mathbf{F} & \mathbf{I} + \mathbf{G} \end{array} \oplus \text{Schur } \mathbf{L}$$

Newton options

Newton-Krylov with Porosity

```
-snes_monitor -snes_converged_reason
-snes_type newtonls -snes_linesearch_type bt
-snes_fd_color -snes_fd_color_use_mat -mat_coloring_type greedy
-ksp_rtol 1.0e-10 -ksp_monitor -ksp_gmres_restart 200
-pc_type fieldsplit
  -pc_fieldsplit_0_fields 0,2 -pc_fieldsplit_1_fields 1
  -pc_fieldsplit_type schur -pc_fieldsplit_schur_precondition selfp
  -pc_fieldsplit_schur_factorization_type full
  -fieldsplit_0_pc_type lu
  -fieldsplit_pressure_ksp_rtol 1.0e-9 -fieldsplit_pressure_pc_type gamg
  -fieldsplit_pressure_ksp_monitor
  -fieldsplit_pressure_ksp_gmres_restart 100
  -fieldsplit_pressure_ksp_max_it 200
```

Early Newton convergence

```

0 TS dt 0.01 time 0
  0 SNES Function norm 5.292194079127e-03
    Linear pressure_ solve converged due to CONVERGED_RTOL its 10
  0 KSP Residual norm 4.618093146920e+00
    Linear pressure_ solve converged due to CONVERGED_RTOL its 10
  1 KSP Residual norm 3.018153330707e-03
    Linear pressure_ solve converged due to CONVERGED_RTOL its 11
  2 KSP Residual norm 4.274869628519e-13
Linear solve converged due to CONVERGED_RTOL its 2
1 SNES Function norm 2.766906985362e-06
  Linear pressure_ solve converged due to CONVERGED_RTOL its 8
  0 KSP Residual norm 2.555890235972e-02
  Linear pressure_ solve converged due to CONVERGED_RTOL its 8
  1 KSP Residual norm 1.638293944976e-07
  Linear pressure_ solve converged due to CONVERGED_RTOL its 8
  2 KSP Residual norm 1.771928779400e-14
Linear solve converged due to CONVERGED_RTOL its 2
  2 SNES Function norm 1.188754322734e-11
Nonlinear solve converged due to CONVERGED_FNORM_RELATIVE its 2
1 TS dt 0.01 time 0.01

```

Later Newton convergence

```
0 TS dt 0.01 time 0.63
  0 SNES Function norm 9.366565251786e-03
    Linear pressure_ solve converged due to CONVERGED_RTOL its 16
    Linear pressure_ solve converged due to CONVERGED_RTOL its 16
    Linear pressure_ solve converged due to CONVERGED_RTOL its 16
  Linear solve converged due to CONVERGED_RTOL its 2
  1 SNES Function norm 4.492625910272e-03
  Linear solve converged due to CONVERGED_RTOL its 2
  2 SNES Function norm 3.666181450068e-03
  Linear solve converged due to CONVERGED_RTOL its 2
  3 SNES Function norm 2.523116582272e-03
  Linear solve converged due to CONVERGED_RTOL its 2
  4 SNES Function norm 3.022638159491e-04
  Linear solve converged due to CONVERGED_RTOL its 2
  5 SNES Function norm 9.761317324448e-06
  Linear solve converged due to CONVERGED_RTOL its 2
  6 SNES Function norm 1.147944474432e-08
  Linear solve converged due to CONVERGED_RTOL its 2
  7 SNES Function norm 8.729160299009e-14
  Nonlinear solve converged due to CONVERGED_FNORM_RELATIVE its 7
1 TS dt 0.01 time 0.64
```

Newton failure

```

0 TS dt 0.01 time 0.64
Time 0.64 L_2 Error: 0.494811 [0.0413666, 0.491642, 0.0376071]
 0 SNES Function norm 9.682733054059e-03
  Linear solve converged due to CONVERGED_RTOL iterations 2
 1 SNES Function norm 6.841434267123e-03
  Linear solve converged due to CONVERGED_RTOL iterations 3
 2 SNES Function norm 4.412420553822e-03
  Linear solve converged due to CONVERGED_RTOL iterations 5
 3 SNES Function norm 3.309326919835e-03
  Linear solve converged due to CONVERGED_RTOL iterations 6
 4 SNES Function norm 3.022494350289e-03
  Linear solve converged due to CONVERGED_RTOL iterations 7
 5 SNES Function norm 2.941050948582e-03
  Linear solve converged due to CONVERGED_RTOL iterations 7
:
:
 9 SNES Function norm 2.631941422878e-03
  Linear solve converged due to CONVERGED_RTOL iterations 7
10 SNES Function norm 2.631897334054e-03
  Linear solve converged due to CONVERGED_RTOL iterations 10
11 SNES Function norm 2.631451174722e-03
  Linear solve converged due to CONVERGED_RTOL iterations 15
:

```

Solver Organization

Preconditioned Newton-Krylov

We can combine Newton-Krylov with Nonlinear CG:

$$(\text{NCG} -_L \text{NRICH}) * (\mathcal{N} \setminus \text{K} -_L \text{NRICH})$$

NCG*Newton options

```
-snes_monitor -snes_converged_reason
-snes_type composite -snes_composite_type multiplicative
-snes_composite_sneses ncg,newtonls
-sub_0_snes_monitor -sub_1_snes_monitor
-sub_0_snes_type ncg -sub_0_snes_linesearch_type cp
-sub_0_snes_max_it 5
-sub_1_snes_linesearch_type bt -sub_1_snes_fd_color
-sub_1_snes_fd_color_use_mat -mat_coloring_type greedy
-sub_1_ksp_rtol 1.0e-10 -sub_1_ksp_monitor -sub_1_ksp_gmres_restart 200
-sub_1_pc_type fieldsplit -sub_1_pc_fieldsplit_0_fields 0,2
-sub_1_pc_fieldsplit_1_fields 1
-sub_1_pc_fieldsplit_type schur
-sub_1_pc_fieldsplit_schur_precondition selfp
-sub_1_pc_fieldsplit_schur_factorization_type full
-sub_1_fieldsplit_0_pc_type lu
-sub_1_fieldsplit_pressure_ksp_rtol 1.0e-9
-sub_1_fieldsplit_pressure_pc_type gamg
-sub_1_fieldsplit_pressure_ksp_gmres_restart 100
-sub_1_fieldsplit_pressure_ksp_max_it 200
```


NCG*Newton convergence

```

0 TS dt 0.01 time 0.64
  0 SNES Function norm 9.682733054059e-03
    0 SNES Function norm 9.682733054059e-03
    1 SNES Function norm 3.705698943518e-02
    2 SNES Function norm 4.981898384331e-02
    3 SNES Function norm 5.710183285964e-02
    4 SNES Function norm 5.476973798534e-02
    5 SNES Function norm 6.464724668855e-02
    0 SNES Function norm 6.464724668855e-02
      0 KSP Residual norm 1.021155502263e+00
      1 KSP Residual norm 9.145207488003e-05
      2 KSP Residual norm 3.899752904206e-09
      3 KSP Residual norm 1.001750831581e-12
    1 SNES Function norm 8.940296814443e-03
  1 SNES Function norm 8.940296814443e-03
  2 SNES Function norm 4.290429277269e-02
  3 SNES Function norm 1.154466745956e-02
  4 SNES Function norm 2.938816182982e-03
  5 SNES Function norm 4.148507767082e-04
  6 SNES Function norm 1.892807106900e-05
  7 SNES Function norm 4.912654244547e-08
  8 SNES Function norm 3.851626525260e-13
1 TS dt 0.01 time 0.65

```

Solver Organization

Full Approximation Scheme

We can use Newton-Krylov as a level solver for FAS:

$$\text{FAS}(\mathcal{N} \setminus K, \mathcal{N} \setminus K)$$

FAS-Newton options

Top level

```

-snes_monitor -snes_converged_reason
-snes_type fas -snes_fas_type full -snes_fas_levels 4
-fas_levels_3_snes_monitor -fas_levels_3_snes_converged_reason
-fas_levels_3_snes_atol 1.0e-9 -fas_levels_3_snes_max_it 2
-fas_levels_3_snes_type newtonls -fas_levels_3_snes_linesearch_type bt
-fas_levels_3_snes_fd_color -fas_levels_3_snes_fd_color_use_mat
-fas_levels_3_ksp_rtol 1.0e-10 -mat_coloring_type greedy
-fas_levels_3_ksp_gmres_restart 50 -fas_levels_3_ksp_max_it 200
-fas_levels_3_pc_type fieldsplit
-fas_levels_3_pc_fieldsplit_0_fields 0,2
-fas_levels_3_pc_fieldsplit_1_fields 1
-fas_levels_3_pc_fieldsplit_type schur
-fas_levels_3_pc_fieldsplit_schur_precondition selfp
-fas_levels_3_pc_fieldsplit_schur_factorization_type full
-fas_levels_3_fieldsplit_0_pc_type lu
-fas_levels_3_fieldsplit_pressure_ksp_rtol 1.0e-9
-fas_levels_3_fieldsplit_pressure_pc_type gamg
-fas_levels_3_fieldsplit_pressure_ksp_gmres_restart 100
-fas_levels_3_fieldsplit_pressure_ksp_max_it 200

```

FAS-Newton options

2nd level

```
-fas_levels_2_snes_monitor -fas_levels_2_snes_converged_reason
-fas_levels_2_snes_atol 1.0e-9 -fas_levels_2_snes_max_it 2
-fas_levels_2_snes_type newtonls -fas_levels_2_snes_linesearch_type bt
-fas_levels_2_snes_fd_color -fas_levels_2_snes_fd_color_use_mat
-fas_levels_2_ksp_rtol 1.0e-10 -fas_levels_2_ksp_gmres_restart 50
-fas_levels_2_pc_type fieldsplit
-fas_levels_2_pc_fieldsplit_0_fields 0,2
-fas_levels_2_pc_fieldsplit_1_fields 1
-fas_levels_2_pc_fieldsplit_type schur
-fas_levels_2_pc_fieldsplit_schur_precondition selfp
-fas_levels_2_pc_fieldsplit_schur_factorization_type full
-fas_levels_2_fieldsplit_0_pc_type lu
-fas_levels_2_fieldsplit_pressure_ksp_rtol 1.0e-9
-fas_levels_2_fieldsplit_pressure_pc_type gamg
-fas_levels_2_fieldsplit_pressure_ksp_gmres_restart 100
-fas_levels_2_fieldsplit_pressure_ksp_max_it 200
```

FAS-Newton options

1st level

```
-fas_levels_1_snes_monitor -fas_levels_1_snes_converged_reason  
-fas_levels_1_snes_atol 1.0e-9  
-fas_levels_1_snes_type newtonls -fas_levels_1_snes_linesearch_type bt  
-fas_levels_1_snes_fd_color -fas_levels_1_snes_fd_color_use_mat  
-fas_levels_1_ksp_rtol 1.0e-10 -fas_levels_1_ksp_gmres_restart 50  
-fas_levels_1_pc_type fieldsplit  
-fas_levels_1_pc_fieldsplit_0_fields 0,2  
-fas_levels_1_pc_fieldsplit_1_fields 1  
-fas_levels_1_pc_fieldsplit_type schur  
-fas_levels_1_pc_fieldsplit_schur_precondition selfp  
-fas_levels_1_pc_fieldsplit_schur_factorization_type full  
-fas_levels_1_fieldsplit_0_pc_type lu  
-fas_levels_1_fieldsplit_pressure_ksp_rtol 1.0e-9  
-fas_levels_1_fieldsplit_pressure_pc_type gamg
```

FAS-Newton options

Coarse level

```
-fas_coarse_snes_monitor -fas_coarse_snes_converged_reason  
-fas_coarse_snes_atol 1.0e-9  
-fas_coarse_snes_type newtonls -fas_coarse_snes_linesearch_type bt  
-fas_coarse_snes_fd_color -fas_coarse_snes_fd_color_use_mat  
-fas_coarse_ksp_rtol 1.0e-10 -fas_coarse_ksp_gmres_restart 50  
-fas_coarse_pc_type fieldsplit  
-fas_coarse_pc_fieldsplit_0_fields 0,2  
-fas_coarse_pc_fieldsplit_1_fields 1  
-fas_coarse_pc_fieldsplit_type schur  
-fas_coarse_pc_fieldsplit_schur_precondition selfp  
-fas_coarse_pc_fieldsplit_schur_factorization_type full  
-fas_coarse_fieldsplit_0_pc_type lu  
-fas_coarse_fieldsplit_pressure_ksp_rtol 1.0e-9  
-fas_coarse_fieldsplit_pressure_pc_type gamg
```

FAS-Newton convergence

```

0 TS dt 0.01 time 0.64
  0 SNES Function norm 9.682733054059e-03
    2 SNES Function norm 4.412420553822e-03
      2 SNES Function norm 8.022096211721e-15
        1 SNES Function norm 2.773743832538e-04
          1 SNES Function norm 5.627093528843e-11
            1 SNES Function norm 4.405884464849e-10
              2 SNES Function norm 8.985059910030e-08
                1 SNES Function norm 4.672651281994e-15
                  0 SNES Function norm 3.160322858961e-15
                    0 SNES Function norm 4.672651281994e-15
                      1 SNES Function norm 1.046571008046e-14
                        2 SNES Function norm 1.804845173803e-02
                          2 SNES Function norm 2.776600115290e-12
                            0 SNES Function norm 1.354009326059e-12
                              0 SNES Function norm 5.881604627760e-13
                                0 SNES Function norm 1.354011456281e-12
                                  0 SNES Function norm 2.776600115290e-12
                                    2 SNES Function norm 9.640723411562e-05
                                      1 SNES Function norm 9.640723411562e-05
                                        2 SNES Function norm 1.057876040732e-08
                                          3 SNES Function norm 5.623618219189e-11
1 TS dt 0.01 time 0.65

```

Solver Organization

Full Approximation Scheme

On fine levels, we can replace Newton-Krylov with
Nonlinear Gauss-Siedel:

$$\text{FAS}(\text{NGS}, \mathcal{N} \setminus \mathbf{K})$$

FAS-NGS options

Top level

```
-snes_monitor -snes_converged_reason  
-snes_type fas -snes_fas_type full -snes_fas_levels 4  
-fas_levels_3_snes_monitor -fas_levels_3_snes_converged_reason  
-fas_levels_3_snes_atol 1.0e-9 -fas_levels_3_snes_max_it 10  
-fas_levels_3_snes_type ngs -fas_levels_3_snes_linesearch_type nleqerr
```

FAS-NGS convergence

```

0 TS dt 0.01 time 0.64
Time 0.64 L_2 Error: 0.494811 [0.0413666, 0.491642, 0.0376071]
  0 SNES Function norm 9.68e-03 [1.96e-03, 1.71e-14, 9.65e-03]
    0 SNES Function norm 9.682733054059e-03
      3 SNES Function norm 9.069944580453e-01
        3 SNES Function norm 3.790367845975e-11
          0 SNES Function norm 1.884126634610e+00
            1 SNES Function norm 6.752057466899e-02
              2 SNES Function norm 3.799909413083e-11
                0 SNES Function norm 1.450032375835e-01
                  1 SNES Function norm 2.567674743706e-04
                    0 SNES Function norm 1.027806561203e+00
                      3 SNES Function norm 1.582489644172e+00
                        1 SNES Function norm 4.847533456932e-01
                          3 SNES Function norm 7.366666076108e-15
                            1 SNES Function norm 1.744390611632e-02
                              3 SNES Function norm 1.473321454964e+00
                                1 SNES Function norm 1.47e+00 [1.44e+00, 2.92e-01, 8.82e-04]
                                  0 SNES Function norm 9.962396109825e+03
                                    1 SNES Function norm 3.189537494940e+86
                                      Nonlinear fas_levels_2_ solve did not converge, DIVERGED_FNORM_NAN
                                        Nonlinear solve did not converge due to DIVERGED_INNER

```

Outline

- 1 Problem Definition
- 2 Solvers for FEM Formulation
- 3 Solvers for FEM+FVM Formulation**

Discretization

Using continuous FE spaces and simple FV,

Q2 velocity

Q1 pressure

FV porosity

which we connect by cell/face interpolants.

```

/* Set discretization object */
if (user->useFV) {
    PetscDSSetDiscretization(prob, 2, fv);
} else {
    PetscDSSetDiscretization(prob, 2, fe[2]);
}
/* Set pointwise residual functions */
PetscDSSetResidual(prob, 2, f0_advection, f1_scalar_zero);
PetscDSSetRiemannSolver(prob, 2, riemann_coupled_advection);

```

Discretization

Using continuous FE spaces and simple FV,

```
-velocity_petscspace_order 2
  -velocity_petscspace_poly_tensor
-pressure_petscspace_order 1
  -pressure_petscspace_poly_tensor
-use_fv
```

which we connect by cell/face interpolants.

```
/* Set discretization object */
if (user->useFV) {
  PetscDSSetDiscretization(prob, 2, fv);
} else {
  PetscDSSetDiscretization(prob, 2, fe[2]);
}
/* Set pointwise residual functions */
PetscDSSetResidual(prob, 2, f0_advection, f1_scalar_zero);
PetscDSSetRiemannSolver(prob, 2, riemann_coupled_advection);
```

Discretization

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/* Set pointwise residual functions */
PetscDSSetResidual(prob, 2, f0_advection, f1_scalar_zero);
PetscDSSetRiemannSolver(prob, 2, riemann_coupled_advection);

```

Solver Organization

Timestepping

We can use a simple split scheme:

$$\nabla p^{k+1} - \nabla \left(\left(\frac{\phi^k}{\phi_0} \right)^{-m} \nabla \cdot \vec{v}^{k+1} \right) - \nabla \cdot \left(2e^{-\lambda(\phi^k - \phi_0)} \dot{\epsilon}^{k+1} \right) = 0$$

$$\nabla \cdot \left(-\frac{R^2}{r_\zeta + 4/3} \left(\frac{\phi^k}{\phi_0} \right)^n \nabla p^{k+1} + \vec{v}^{k+1} \right) = 0$$

$$\frac{\phi^{k+1} - \phi^k}{\Delta t} - \nabla \cdot (1 - \phi^k) \vec{v}^{k+1} = 0$$

Solver Organization

Timestepping

Or one that couples the algebraic and evolution equations:

$$\nabla p^{k+1} - \nabla \left(\left(\frac{\phi^{k+1}}{\phi_0} \right)^{-m} \nabla \cdot \vec{v}^{k+1} \right) - \nabla \cdot \left(2e^{-\lambda(\phi^{k+1} - \phi_0)} \dot{\epsilon}^{k+1} \right) = 0$$

$$\nabla \cdot \left(-\frac{R^2}{r_\zeta + 4/3} \left(\frac{\phi^{k+1}}{\phi_0} \right)^n \nabla p^{k+1} + \vec{v}^{k+1} \right) = 0$$

$$\frac{\phi^{k+1} - \phi^k}{\Delta t} - \nabla \cdot (1 - \phi^k) \vec{v}^{k+1} = 0$$

Newton options

```
-snes_atol 1.0e-10 -snes_monitor_field -snes_converged_reason  
-snes_linesearch_type basic -snes_fd_color -snes_fd_color_use_mat  
-mat_coloring_type greedy -mat_coloring_greedy_symmetric 0  
-ksp_rtol 1.0e-10 -ksp_monitor -ksp_gmres_restart 200  
-pc_type fieldsplit  
-pc_fieldsplit_0_fields 0,2 -pc_fieldsplit_1_fields 1  
-pc_fieldsplit_type schur -pc_fieldsplit_schur_precondition selfp  
-pc_fieldsplit_schur_factorization_type full  
-fieldsplit_0_ksp_rtol 1.0e-8 -fieldsplit_0_pc_type lu  
-fieldsplit_pressure_ksp_rtol 1.0e-9 -fieldsplit_pressure_pc_type svd
```

Early Newton convergence

```
5 TS dt 0.005 time 0.025
  0 SNES Function norm 6.52e-02 [1.46e-14, 4.91e-16, 6.52e-02]
    0 KSP Residual norm 4.26e-04
      1 KSP Residual norm 1.78e-17
    1 SNES Function norm 2.19e-03 [2.96e-08, 3.91e-09, 2.19e-03]
    2 SNES Function norm 7.51e-05 [3.40e-11, 4.55e-12, 7.51e-05]
    3 SNES Function norm 2.58e-06 [2.46e-13, 1.28e-14, 2.58e-06]
    4 SNES Function norm 8.86e-08 [1.39e-14, 6.64e-16, 8.86e-08]
6 TS dt 0.005 time 0.03
```

Late Newton convergence

```

0 TS dt 0.005 time 0.825
  0 SNES Function norm 2.14e+00 [ 1.40e-14, 3.67e-16, 2.14e+00]
  0 KSP Residual norm 3.53e-01
  1 KSP Residual norm 1.03e-10
  2 KSP Residual norm 2.82e-16
  1 SNES Function norm 5.13e-02 [ 2.01e-04, 1.47e-04, 5.13e-02]
  2 SNES Function norm 2.47e-02 [ 9.20e-06, 7.73e-06, 2.47e-02]
  3 SNES Function norm 7.81e-03 [ 2.13e-06, 1.67e-06, 7.81e-03]
  4 SNES Function norm 2.12e-03 [ 1.81e-07, 1.41e-07, 2.12e-03]
  5 SNES Function norm 4.72e-04 [ 1.08e-08, 8.28e-09, 4.72e-04]
  6 SNES Function norm 1.12e-04 [ 5.76e-10, 4.41e-10, 1.12e-04]
  7 SNES Function norm 2.63e-05 [ 3.21e-11, 2.50e-11, 2.63e-05]
  8 SNES Function norm 6.17e-06 [ 1.77e-12, 1.26e-12, 6.17e-06]
  9 SNES Function norm 1.45e-06 [ 1.07e-13, 9.84e-14, 1.45e-06]
 10 SNES Function norm 3.40e-07 [ 1.78e-14, 4.74e-15, 3.40e-07]
 11 SNES Function norm 7.99e-08 [ 1.36e-14, 1.88e-15, 7.99e-08]
 12 SNES Function norm 1.88e-08 [ 1.34e-14, 5.72e-16, 1.88e-08]
1 TS dt 0.005 time 0.83

```

FAS-Newton options

Top level

```
-snes_atol 1.0e-9 -snes_monitor_field -snes_converged_reason
-snes_type fas -snes_fas_type full -snes_fas_levels 3
  -fas_levels_2_snes_monitor -fas_levels_2_snes_converged_reason
  -fas_levels_2_snes_atol 1.0e-9 -fas_levels_2_snes_max_it 2
  -fas_levels_2_snes_type newtonls
  -fas_levels_2_snes_linesearch_type basic
  -fas_levels_2_snes_fd_color -fas_levels_2_snes_fd_color_use_mat
  -fas_levels_2_ksp_rtol 1.0e-10 -fas_levels_2_ksp_gmres_restart 50
  -fas_levels_2_pc_type fieldsplit
  -fas_levels_2_pc_fieldsplit_0_fields 0,2
  -fas_levels_2_pc_fieldsplit_1_fields 1
  -fas_levels_2_pc_fieldsplit_type schur
  -fas_levels_2_pc_fieldsplit_schur_precondition selfp
  -fas_levels_2_pc_fieldsplit_schur_factorization_type full
  -fas_levels_2_fieldsplit_0_pc_type lu
  -fas_levels_2_fieldsplit_pressure_ksp_rtol 1.0e-9
  -fas_levels_2_fieldsplit_pressure_pc_type svd
  -fas_levels_2_fieldsplit_pressure_ksp_gmres_restart 100
  -fas_levels_2_fieldsplit_pressure_ksp_max_it 200
```

FAS-Newton options

Coarse level

```
-fas_coarse_snes_max_it 10 -fas_coarse_snes_max_linear_solve_fail 10
-fas_coarse_snes_atol 1.0e-9
-fas_coarse_snes_monitor -fas_coarse_snes_converged_reason
-fas_coarse_snes_type newtonls -fas_coarse_snes_linesearch_type bt
-fas_coarse_snes_fd_color -fas_coarse_snes_fd_color_use_mat
-fas_coarse_ksp_rtol 1.0e-10 -fas_coarse_ksp_gmres_restart 50
-fas_coarse_pc_type fieldsplit
-fas_coarse_pc_fieldsplit_0_fields 0,2
-fas_coarse_pc_fieldsplit_1_fields 1
-fas_coarse_pc_fieldsplit_type schur
-fas_coarse_pc_fieldsplit_schur_precondition selfp
-fas_coarse_pc_fieldsplit_schur_factorization_type full
-fas_coarse_fieldsplit_0_pc_type lu
-fas_coarse_fieldsplit_pressure_ksp_rtol 1.0e-9
-fas_coarse_fieldsplit_pressure_pc_type svd
```

FAS-Newton convergence

```

0 TS dt 0.005 time 0.825
  0 SNES Function norm 2.14e+00 [1.40e-14, 3.67e-16, 2.14e+00]
  0 SNES Function norm 2.136811983007e+00
  2 SNES Function norm 2.467490038458e-02
    0 SNES Function norm 2.892788645925e-02
    5 SNES Function norm 6.686368379854e-11
  0 SNES Function norm 5.034219273717e-02
  1 SNES Function norm 1.054842559307e-03
    0 SNES Function norm 1.663080254945e-03
    4 SNES Function norm 2.126370356882e-10
  0 SNES Function norm 2.599480303180e-03
  1 SNES Function norm 9.990047497418e-05
  0 SNES Function norm 4.798584798600e-02
  2 SNES Function norm 1.288870672992e-03
    1 SNES Function norm 3.770621359658e-05
      2 SNES Function norm 1.127970439777e-08
    1 SNES Function norm 1.008431552413e-06
  0 SNES Function norm 2.502531975042e-03
  2 SNES Function norm 4.730240156687e-05
  1 SNES Function norm 4.73e-05 [1.04e-10, 7.85e-11, 4.73e-05]
  2 SNES Function norm 3.98e-09 [1.38e-14, 4.18e-16, 3.98e-09]
1 TS dt 0.005 time 0.83

```

FAS-NGS options

Top level

```
-snes_atol 1.0e-9 -snes_monitor_field -snes_converged_reason  
-snes_type fas -snes_fas_type full -snes_fas_levels 3  
  -fas_levels_2_snes_monitor -fas_levels_2_snes_converged_reason  
  -fas_levels_2_snes_atol 1.0e-9 -fas_levels_2_snes_max_it 10  
  -fas_levels_2_snes_type ngs -fas_levels_2_snes_linesearch_type bt
```

FAS-NGS convergence

0 TS dt 0.005 time 0.825

0	SNES	Function norm	2.14e+00	[1.39e-14,	3.66e-16,	2.13e+00]
1	SNES	Function norm	2.87e-04	[2.08e-04,	4.80e-06,	1.98e-04]
2	SNES	Function norm	3.15e-05	[2.30e-05,	9.56e-07,	2.19e-05]
3	SNES	Function norm	1.65e-05	[1.14e-05,	5.44e-07,	1.21e-05]
4	SNES	Function norm	1.07e-05	[7.38e-06,	3.48e-07,	7.89e-06]
5	SNES	Function norm	7.06e-06	[4.85e-06,	2.26e-07,	5.20e-06]
6	SNES	Function norm	4.67e-06	[3.20e-06,	1.48e-07,	3.44e-06]
7	SNES	Function norm	3.09e-06	[2.12e-06,	9.82e-08,	2.27e-06]
8	SNES	Function norm	2.05e-06	[1.40e-06,	6.52e-08,	1.50e-06]
9	SNES	Function norm	1.36e-06	[9.35e-07,	4.34e-08,	1.00e-06]
10	SNES	Function norm	9.03e-07	[6.21e-07,	2.89e-08,	6.64e-07]
11	SNES	Function norm	6.00e-07	[4.13e-07,	1.94e-08,	4.41e-07]
12	SNES	Function norm	3.99e-07	[2.75e-07,	1.30e-08,	2.94e-07]
13	SNES	Function norm	2.67e-07	[1.84e-07,	8.84e-09,	1.96e-07]
14	SNES	Function norm	1.78e-07	[1.23e-07,	6.01e-09,	1.31e-07]
15	SNES	Function norm	1.20e-07	[8.31e-08,	4.12e-09,	8.80e-08]
16	SNES	Function norm	8.12e-08	[5.64e-08,	2.85e-09,	5.94e-08]
17	SNES	Function norm	5.55e-08	[3.87e-08,	1.99e-09,	4.05e-08]
18	SNES	Function norm	3.86e-08	[2.70e-08,	1.41e-09,	2.80e-08]
19	SNES	Function norm	2.74e-08	[1.93e-08,	1.01e-09,	1.97e-08]
20	SNES	Function norm	2.00e-08	[1.43e-08,	7.48e-10,	1.44e-08]

1 TS dt 0.005 time 0.83

What does this mean?

- PETSc allows comparison between
Meshes,
Discretizations, and
Solvers
- Can allow more robust, scalable solves
- Can allow better physical fidelity

<http://www.mcs.anl.gov/petsc>

What does this mean?

There are a bunch of unanswered analytical questions:

- Is the hybrid method stable? Working on a proof.
- Can we use the Implicit-Input/Explicit-Output scheme to increase the timestep?
- What is the accuracy/degree of freedom?

<http://www.mcs.anl.gov/petsc>